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fuel cell work
(NASA contract
NAS 3-2551)

ti MONTHLY PROGRESS REPORT

No. 8

for *6*

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15 Mar.

February, 61963

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(NASA CR-55695) OTS;
development...

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NEW PRODUCT RESEARCH of TAPCO

OTS PRICE

XEROX

\$ 4.60 *ph*

MICROFILM

\$ 6.64 *mf*

March 15, 1963

I INTRODUCTION

This document represents the eighth monthly report covering the work on the experimental program for development of an "Osmotic Still" and improvements in the performance characteristics of the Ionics Dual Membrane Fuel Cell during the month of February 1963. This development work is being accomplished under NASA-Lewis Research Center Contract No. NAS 3-2551 by the New Product Research Department of TAPCO, and Ionics Inc. as a subcontractor to TAPCO.

II OVERALL PROGRESS

A. Tapco Portion of Program

1. Ionac membranes MC 3142, MA 3148, XLMA 3236, and XLMC 3235 were tested for liquid leakage at room temperature after being soaked in water at room temperature for 16 hours. All but the XLMC 3235 showed no leakage with a pressure difference of 16 psi. The XLMC 3235 leaked with a 15 psi pressure difference.

2. The same membranes were pressure tested at room temperature after being pretreated in 180°F (recommended by Ionac) water for four hours. All membranes leaked excessively at pressure differences from 2 to 10 psi.

3. Performance tests were attempted with the MC 3142 and the MA 3148. The MC 3142 was pretreated in 180°F water before installation and excessive leakage occurred immediately upon evacuation of the vapor chamber before acid heatup.

The MA 3148 was run for approximately four hours at temperatures of 125°F and 140°F, but extremely small amounts of liquid were extracted during this period and a pH was never exceeded. Thus, the above Ionac membranes were determined unsuitable and testing of these membranes was discontinued.

4. Five successful test runs were completed with the AMF C-60 membrane at temperatures from 150°F to 200°F and at vapor pressures from .45 psia to 1.23 psia with an acid concentration of 25.2%.

5. A total of 15 successful test runs were made with the AMF C-60 membrane at 200°F and acid concentrations from 15.2% to 60%.

6. Two tests on this membrane were made with acid pressures of 26 psia and 32 psia at 200°F and 25.2% concentration.

7. The AMF C-60 membranes used in the tests during this reporting period are the same membranes used during the last reporting period and the Kel-F coated support screens have been used throughout all the tests and appears to be in good condition.

8. Porous Kel-F and porous polyethylene were leak tested as non-wetting materials, but were determined as unsatisfactory.

B. Ionics Portion of Program

1. Progress was made in the areas of test rig control and operation, membrane and electrode screening, successful life testing, delineation of the source of liquid in the cell gas streams, determination of the effect of gas circulation rates on cell performance, finalizing the design of and expediting procurement of materials for the multiple cell batteries.

2. Revamping of test rig controls and operation has led to successful long-term tests of fuel cells without any premature failures.

3. Continued screening tests in small (4 sq. in.) test cells reinforced the finding that we are now using the best membranes (IONICS 61-AZG and 61-AZL) and electrodes (platinum black sintered with teflon) that are available.

4. Long successful runs of single cells - up to 500 hours and still running - have been achieved while meeting the electrical output requirements.

5. The liquid appearing in the gas streams was shown definitely to have come through the membranes. Rates of liquid appearance were determined.

6. Wide variation in gas rates was shown to have no effect on cell output, thus simplifying eventual system control problems. The pressure drop through a single cell was shown to be small even at gas circulation rates 20 times the consumption rate - indicating that power losses for gas circulation will not be serious.

7. Design modifications based on our findings were made and finalized design drawings for multiple-cell battery components prepared. Procurement and fabrication is in full swing.

II. CURRENT PROBLEMS

A. Tapco Portion of Program

There have been no major problems during this reporting period.

B. Ionics Portion of Program

1. Delivery of ordered materials and fabrication of components needs additional expediting.

IV NEXT MONTH'S EFFORT

A. Tapco Portion of Program

1. Complete performance tests on the AMF C-60 membrane.
2. Select design point for 2 KW still design and make preliminary gasket tests for 2 KW design.
3. Design 2 KW still and test rig.

B. Ionics Portion of Program

1. Expedite receipt of ordered materials.
2. Complete fabrication of all components for 5-cell batteries.
3. Complete modifications to test rig to permit testing 5-cell batteries.
4. Finalize technique for assembling, venting and filling multiple-cell batteries.
5. Assemble initial two 5-cell batteries.

V TEST RESULTS

A. Tapco Portion of Program

1. The initial test with the Ionac MC 3142 membrane was made in the test unit after the membranes had been soaked in 180°F water for four hours (recommended by Ionac representative). Upon initial evacuation of vapor chamber prior to acid heatup, the membrane leaked acid excessively with a vacuum of only 20 cm mercury. Upon removal of the membrane from the test unit, inspection showed no rupture in the membrane.
2. Leakage tests were made on the Ionac membranes after soaking in room temperature water for 16 hours. These tests were made by securing the membrane over a 3/8" diameter hole and exposing one side of the membrane to pressurized water and the other side of the membrane to atmospheric air. Leakage was determined by visual observation. The water pressure was gradually increased to determine where leakage was visible.

<u>Membrane</u>	<u>Water Pressure</u>	<u>Pressure Duration</u>	<u>Results</u>
MC 3142	16 psig	16 hrs	No leakage
MA 3148	16 psig	1 hr	No leakage
XLMA 3236	16 psig	1 hr	No leakage
XLMC 3235	15 psig	1 hr	Small leakage at first but increased with time

3. Leakage tests were made on the same membranes after soaking in 180°F water for four hours.

<u>Membrane</u>	<u>Water Pressure</u>	<u>Results</u>
MC 3142	2 psig	Rapid leakage
MA 3148	10 psig	Small leakage
XLMA 3236	8 psig	Rapid leakage
XLMC 3235	3 psig	Rapid leakage

4. Leak tests were made on two non-wetting porous materials. A sample of porous Kel-F sheet with pore size under 7 microns and a sample of porous polyethylene sheet with pore size under 2.0 microns were obtained from the ESB Reeves Corporation. The tests were made with water at room temperature.

<u>Sample</u>	<u>Results</u>
Porous Kel-F	Leaked at 7 psig
Porous Polyethylene 13-CN	Leaked at 3.5 psig

5. Attached are plotted data obtained on the AMF C-60 to date. (TRW Fig. 1A) Also, attached are performance test raw data for this reporting period.

B. Ionics Portion of Program

1. Test Rig Revamp

Many cells previously had to be taken off test prematurely due to malfunction of the test rig control system. The test rig and test procedures were revamped and no premature (less than 100 hour)

malfunction has occurred since. The major changes included:

1. Operation at 5 psig instead of 15 psig.
2. Additional instrumentation to ensure that the pressure in each gas compartment and each electrolyte compartment was 5 ± 0.3 psig.
3. Gas manifold changes to ensure that gas pressure remained constant during gas supply changes.
4. Additional operator instruction to ensure that the pressure differential between gas and electrolyte compartments did not exceed 1.5 psi during startup.
5. All tygon tubing in the oxygen system has been replaced with polyethylene to prevent the occasional fires which had been noticed in these lines.

2. Single 4 sq. in. Cell Studies

2.1 Membrane Studies

The effect of various membranes on cell resistance was investigated at Ionics and as part of a subcontract at Arthur D. Little. In addition, the appearance rate of liquid in the gas compartments was measured in the cells tested at Ionics.

Six different types of membranes were studied at Ionics: 61AZG (Ionics Standard), 61-DYG, 61-AZL, 61-AZL-15, 61-AZL-8, and AMF-C313. The 61-AZG, AMF C-313 and AMF C-60 were studied at A.D.L. Hydrogen and oxygen were bubbled through 6N H₂SO₄ prior to being fed to the cells so as to saturate the gases with water vapor. Liquid coming out of the two gas compartments was collected in small graduated cylinders. Standard sintered electrodes were used in these cells. Results obtained are summarized in Table 1. The relative cell resistances were obtained from the slope of current vs. voltage plots. All the cells were run at a current of 400 ma, except when current vs. voltage curves were being obtained. Cells containing 61-AZL and 61-AZG showed the lowest resistance - 0.26 and 0.31 ohms, corresponding to cell specific conductances of 138 and 116 mhos/ft². This may be compared to values up to 140-180 mhos/ft² found for the 36 sq. in cells. The larger cells may be showing a higher specific conductance because the electrolyte compartments are thinner:

0.060" in the 36 sq. in. cells vs. 0.625" in the 4 sq. in. cells. The amount of liquid collected was very low and varied from negligible to 1.5 ml per day compared to 3.2 ml/day produced from the fuel cell reaction.

Overall, 61-AZG appears the most desirable membrane with 61-AZL a possible second. The AMF membranes had previously shown considerably poorer stability than 61-AZG or 61-AZL on continued exposure to 6N sulfuric acid at elevated temperatures.

2.2 Electrode Studies

Several different types of electrodes were tested at Ionics and under subcontract at Arthur D. Little.

2.2.1 Clevite Electrodes

Clevite Corporation made two electrodes (sintered type) using a lighter grade of MgO powder in the paste. Performance of these electrodes was very poor and voltages were taken only at 0.4 and 0.67 amps.

AMPS	- - - - - VOLTS - - - - -		
	TOTAL	H ₂	O ₂
0.4	0.407	0.147	0.263
0.67	0.313	0.100	0.207

These voltage readings were considerably lower than voltages obtained from the sintered electrode used before: e.g., 0.76 total volts at 0.4 amps. These new electrodes were pressed at a very high pressure (10,000 psi compared to our normal 4000 psi). This might have caused low porosity, resulting in low meter readings.

2.2.2 Mott Electrodes

Mott Metallurgical Corporation prepared sintered platinum black electrodes. These are circular and have an area of 2.95 sq. in. A characterization curve is shown in Figure 1. The values obtained here are also very low: 0.4 total

volts at 0.4 amps. The cell had a specific conductance of 120 mhos/ft². The oxygen electrode was sprayed with teflon and then tried in the cell. The performance of this cell was even poorer than the above. Current more than 80 ma could not be drawn.

2.2.3 Imprinted Electrodes (ADL)

It appeared first that a technique of imprinting the membrane with Pt black would improve the catalyst membrane contact as experiments of this type had been performed by Gregor⁽¹⁾, ⁽²⁾ with some success. Series 100 AMF membranes had been subjected to 60,000 psi and 115°C to imbed Pt black and had performed well in single membrane cells with no free electrolyte. However, further experiments reported by Perry⁽³⁾ in which imprinted cation membranes were used in a dual membrane alkaline cell gave polarization curves no higher than those reported by Lurie et al.⁽⁴⁾ for similar cells with unimprinted Ionics membranes. Attempts to imprint both Ionics and AMF membranes at lower temperatures (to prevent membrane drying) had proved unsuccessful and were discontinued in the light of Perry's report.

2.2.4 Deposited Electrodes (ADL)

Chemical reduction of platinum compounds to metal in and on the membrane was attempted in an effort to put more active catalyst in intimate contact with the membrane. The soluble Pt (NH₃) Cl₂ complex was prepared by treating a chloroplatinic acid solution with excess ammonia and the membrane surface washed with this solution. The membrane was then flushed with a basic solution of sodium borohydride, reducing the complex to finely-divided platinum and various soluble salts. While a darkening of the membrane was observed which could be attributed to the presence of platinum, it was not possible to build up any appreciable concentration at the surface of the membrane, the only area in which it would be accessible to gaseous H₂ and so useful as a catalyst.

An attempt was also made to use this impregnated membrane as a cathode and deposit upon it electrochemically Pt black from standard platinizing solutions. This also proved unsatisfactory as no significant current density could be obtained, showing that even with reduced platinum present, the surface of the membrane was still not the electronic conductor required for this technique.

2.2.5 Pure Platinum Electrodes (ADL)

The presence of Teflon in the Pt paste has seemed a possible source of trouble as it places an electrically insulating material in the electrode-catalyst region. Taschek and Wynn⁽⁵⁾ report that it may introduce as much as 70 mv additional ohmic polarization when used as wet-proofing material in place of the more common but less durable paraffin. A fuel cell was prepared in which a thin layer of pure Pt black was sandwiched between membranes and electrodes, the electrodes having been well coated with Pt black electrochemically. The polarization curve is shown in Figure 2. After four days it showed no deterioration due to lack of wet-proofing although this would certainly have become a problem at a later time. The conclusions to be drawn from these curves is that at the low current densities concerned, about 700 ma for the small cell, voltage loss is due in overwhelming part to the initial electrode polarization and efforts to reduce the limiting slope have little effect upon the immediate application of the cell. Reports from Ionics concerning a cell with teflon present primarily on the oxygen side give a limiting slope of about 0.2 ohms for the cell but a voltage at 700 ma again of about 0.65 v, the same voltage is obtained both with and without teflon. The problem is thus one of catalysis rather than internal resistance of the cell components. Further work should then be concerned with this problem.

2.2.6 Platinized Carbon Electrodes (ADL)

As one step toward investigation of the catalysis problem, a pair of platinized carbon electrodes were prepared according to the method of Taschek and Wynn⁽⁵⁾. Two 2' x 2" x 3/32" pieces of PC 57, manufactured by the Stackpole Carbon Company, were chosen. This material has a porosity of 1.07 cc/g and surface area of about 300M²/g. Pores range from 3 to 7 microns in diameter. These blocks were wet-proofed by soaking in a solution of 2 g paraffin in 100 ml petroleum ether, dried, and then heated to 200°C for two hours. While still hot, they were painted with a 10% solution of H₂PtCl₄, using enough solution for a coverage of 2 mg Pt/cm². They were then dried in an oven at 100°C for several hours and transferred to a vacuum oven at 150°C for five more hours to decompose the platinum compound.

The prepared carbon was put into the cell with the treated surface against the membrane and electrical contact was made by platinum gauze pressed against the back of the carbon. Resistance of the assembled cell was 0.4 ohm, measured with a Kiethley Model 502 Multiohmeter. A polarization curve for this electrode system is also shown in Figure 2.

2.2.7 Bibliography for ADL Electrode Study

1. H. P. Gregor, "Fuel Cell Materials," Fifth Quarterly Progress Report, Contract No. DA-36-039 SC-85-85384.
2. H. P. Gregor, "Fuel Cell Materials," Final Report, Contract No. DA-36-039 SC-85384.
3. J. Perry, Jr., Proceedings 16th Annual Power Sources Conf. (1962).
4. R. M. Lurie, C. Berger and R. J. Schuman, "Fuel Cells," Vol. 11, Reinhold, p. 143, (1963).
5. W. G. Taschek and J. E. Wynn, Proceedings 16th Annual Power Sources Conf. (1962).

3. Single 36 Sq. In. - Cell Studies

Two cells with tantalum pusher and separator plates are operating very well at 5 psig. For one of these cells, the effect of wide variations in gas rates on pressure drop and polarization curves were determined. The rate of liquid appearance in the gas compartments was also checked. Two unusual cells were placed on stream to help pin down the source of the liquid found in the gas compartments.

Detailed results are given in Table 2.

3.1 Effect of Pressure Level

Cell E-1282 and Cell E-1268 were identical cells except that E-1268 was run at a nominal 16 psig and E-1282 at a nominal 5 psig. As reported last month, when 4 amps were drawn from E-1268, the cell voltage did not maintain its initial value of 0.79 v but fell to 0.632 v in 120 hours. The lower pressure E-1282 on the other hand maintained voltage very well - reading 0.748v after 288 hours. This improved voltage maintenance was ascribed to smoother operation of the cell at the lower pressure level. Unfortunately, the hydrogen flow path became obstructed after approximately 300 hours: hydrogen would no longer flow through the cell and the cell failed. Inspection of the cell after dismantling did not disclose the nature nor exact location of the blockage.

3.2 Effect of Well-Balanced Pressures

In view of the improvement in operation obtained by reduction of the pressure level (Cell E-1282), a cell was put on stream with particular effort to keep inter-compartment pressure differences during startup and operation to a minimum (Cell E-1651). This cell has maintained a voltage of close to 0.8v at 4 amps for over

500 hours. The polarization curves obtained after 168 hours are produced in Figure 3. Note that the hydrogen electrode suffers from "concentration polarization" at about 50 amps/ft² while the oxygen is unaffected at this current density. The tantalum pusher and separator plates in this cell appear to be giving excellent service.

The specific conductance of the cell showed a continuing slow decrease with time, as have all other cells. It is not currently clear whether this is due to gradual membrane fouling, electrode deterioration or some other degradative process.

3.3 Source of Liquid in Gas Compartments

To determine the source of the liquid observed in the gas chambers and in the gas outlet lines in a qualitative way, two unusual cells were built. The first cell (E1279) had non-permeable pieces of rubber in place of membranes. This would allow leakage from the electrolyte ducts, hopefully to the same extent as in the regular cell, but would prevent transport of liquid through the membrane.

The second cell (E-1652) had an electrolyte chamber isolated from the gas compartments so that liquid could only reach the gas compartments by passing through the membrane. Liquid collection bottles were provided for all exiting gas streams of both cells.

After three weeks operation, the quantity of acid found in the collection bottles of the cell with the impermeable membrane-substitutes was equivalent to only 4 cc of electrolyte on the oxygen side and 12 cc on the hydrogen side. This demonstrated that with the present gasketing system, the acid leakage between compartments by way of the manifolds, ports, etc., can be kept to negligible levels. On the other hand, the collector bottles on each of the gas streams leaving the cell with the external electrolyte flow circuit (E-1652) had collected several hundred cc's of liquid during the same three week period. The liquid had definitely passed through the membrane.

3.4 Rate of Liquid Appearance

The rate of liquid production from the gas compartments were measured on cell D9228. These data are presented in Figure 4. The average sulfuric acid concentration in the liquid collected in the hydrogen side is 6N and in the oxygen side is 4.5N. The data presented are after 24 hours of operation when the cell had achieved reasonably steady operation. By taking the slope of the curve, an average value for the rate of liquid production can be obtained. The hydrogen side curve produces a consistent 0.6 ml/hr; the oxygen side was less consistent (possibly due to intermittent liquid holdup) but an average value of 0.63 ml/hr can be obtained. The rate of water production by reaction is 1.35 ml H₂O/hr.

3.5 Effect of Varying Gas Rates

Pressure drops across the gas compartments were measured for various gas flow rates in cell D9228. These data appear in Figure 5. At 5 psig and 25°C, the cell uses 22 ml/min of hydrogen and half the quantity of oxygen at four amperes. At twenty times these gas rates, the pressure drops were only 30 mm H₂O on the O₂ side and 20 mm H₂O on the H₂ side. The energy loss even at very high gas recycle rates would thus be quite low. Polarization curves were also measured on cell D9228 with carefully controlled flow rates to determine the influence of gas flow rate on cell performance. Flow rates of 140 and 500 ml/min on the hydrogen side, and 50 and 200 ml/min on the oxygen side were compared. The polarization curves, Figure 6, show no detectable difference up to a total current of 10 amperes (40 amp/ft²). These measurements will be extended to 25 amperes.

4. Multi-Cell Battery Design Modifications

In the light of results with single cells, design modifications have been made in the radial porting of the gas and electrolyte compartments.

4.1 Gas Compartments

In the case of the gas compartments, the object has been to reduce the chance of gas-electrolyte leakage and to obtain better gas distribution to the parallel-connected cells. To this end, the minimum distance between the radial gas ports and the electrolyte port has been increased from 5/16" to 1/2". In addition, the number of inlet ports has been reduced to one, and its width reduced from 0.060 in. to 0.030 in. with the object of producing a higher hydraulic pressure drop and thus better gas distribution.

4.2 Electrolyte Compartment

With these components, the cut-and-cover technique for forming the radial electrolyte channels has been replaced by drilling a simple hole. It has proved difficult to maintain surface smoothness tolerances with the previously used, glued compartments. To permit the use of a drilled port it has been necessary to increase the thickness of the compartment from 0.060" to 0.100". In the case of the exit channel at the top of the cell, two parallel holes have been included to reduce the possibility of blockage by a gas bubble. (See Drawing number 2). A single inlet port with a cross-sectional area of about 0.0008 sq. in. will replace the two former inlet ports which had a joint cross-sectional area of 0.0036 sq. in. This was done to increase the hydraulic resistance and thus the efficiency of electrolyte manifolding.

5. Multiple-Cell Battery Component Procurement

5.1 Gas and Electrolyte Compartments

It has been decided to make at least one 5-cell battery out of Halon and one out of Penton. Because of the long delivery period for the non-standard thickness required for the electrolyte compartment, sufficient material has been ordered to permit the construction of a 10-cell battery in either plastic. Delivery has been promised for 15 March 1963.

5.2 Gasketing

From corrosion studies, it is expected that Dacron-reinforced Viton will prove to be a superior gasketing material. However, it has not been employed extensively in single cells as has Buna N. For this reason, it has been thought advisable to have a reserve stock of Buna N gaskets, which, though not ideal, would be expected to last the 100 hour life requirements of the batteries.

5.3 Electrode Manufacture

New plattens have been designed and materials ordered for their fabrication. The new plattens will permit the making of electrodes with one pressing operation in place of two, thus presumably permitting production of more reproducible electrodes.

5.4 Pusher and Separator Plates

Corrosion studies have shown tantalum to be the most resistant metal (other than platinum) to corrosion in 6N H₂SO₄. However, both niobium and zirconium have promisingly low corrosion rates. Since both these metals are less costly and lighter than the tantalum, it was decided to assemble at least one 5-cell battery containing some cells made with each metal.

5.5 General Status

The present state of procurement situation is summarized in Table 3. The technical task status and schedule is appended to the letter regarding manhours, dollar expenditures and commitments attached to this report.

Fig. TRW 1A

OSMOTIC STYLL TEST RESULTS

Water Extraction Rate vs. Vapor Pressure Difference
for the AMP C-60 Membrane.
Test Results through Feb. 28, 1963

Notation:

ΔP - Vapor pressure difference between H_2SO_4 solution, vapor pressure at temperature and the test vapor pressure.

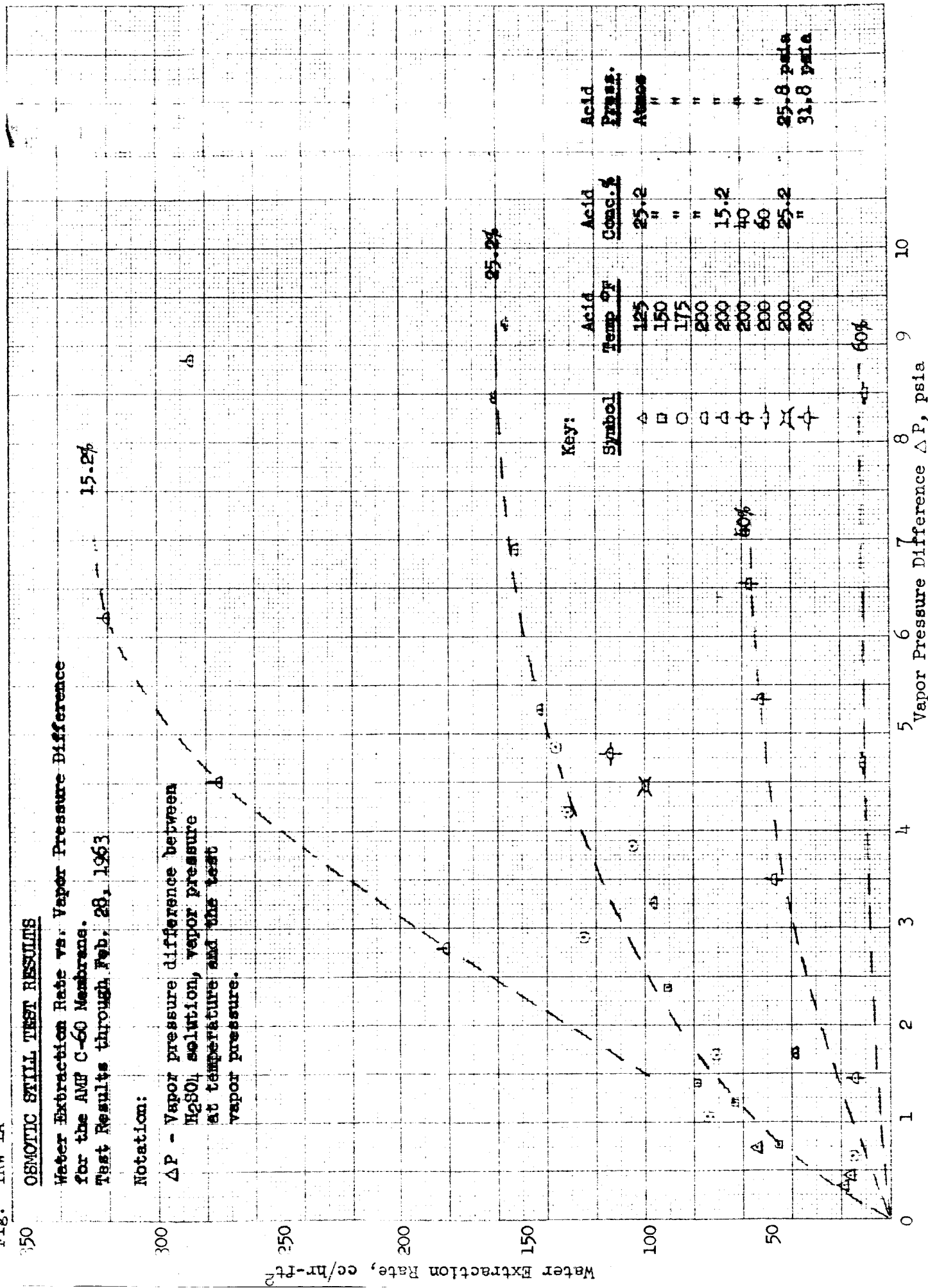


TABLE I
MEMBRANE STUDY - 4 SQ. IN. CELLS - 25°C

Cell No.	Membrane Type	Cell Resistance Ohms	Cell Specific Conductance mhos/ft ²	Liquid Collected, mls/day	
				H ₂ Side	O ₂ Side
E 0224	61-AZG	0.31	116	negligible	0.13
ADL-11	61-AZG	0.27	135	*	*
E 1325	61-DYG	0.45	80	0.14	0.29
E 1327	61-AZL	0.26	138	1.44	2.6**
E 1326	61-AZL-15	0.45	80	0.56	1.17
E 1330	61-AZL-8	0.38	95	0.16	0.12
E 1331	AMF-C-313	0.33	109	0.03	0.03
ADL-12	AMF-C-313	0.35	104	*	*
ADL-13	AMF-C-60	0.38	95	*	*

* Not measured at A.D.L.

** On dye test, the membrane showed a pinhole.

FIGURE 1

CHARACTERIZATION
MOTT CURVE FOR
2.95 IN² AREA

$R = 0.41 \Omega$

SPECIFIC CONDUCTANCE = 120 MHOS/FT^2

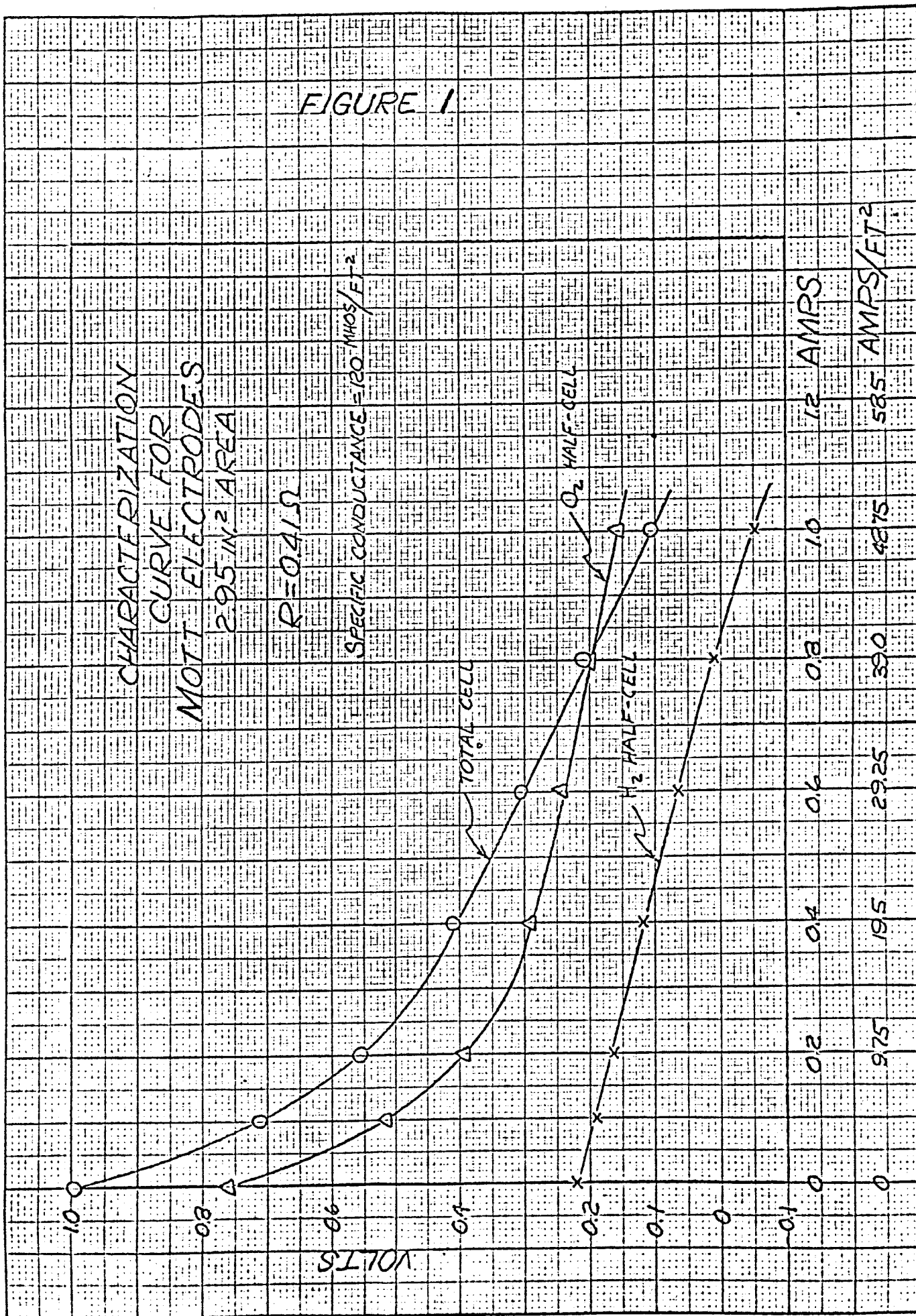


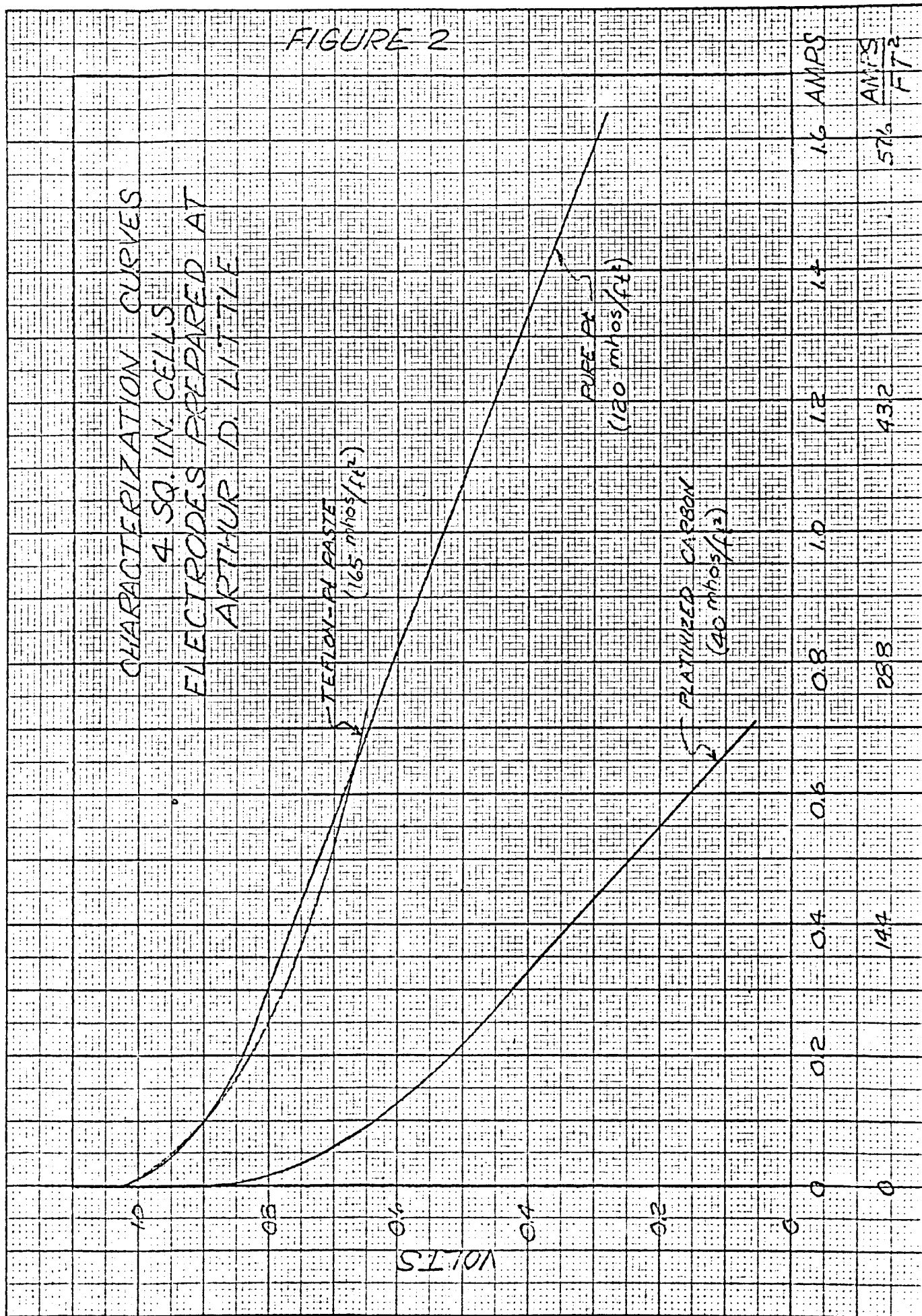
FIGURE 2

CHARACTERIZATION CURVES
4 SQ. IN. CELLS
ELECTRODES PREPARED AT
ARTHUR D. LITTLE

TERION-PL PASTE
(165 mhos/cm²)

PURE PL
(120 mhos/cm²)

PLATINIZED CARBON
(40 mhos/cm²)



AMPS
576
F²

432

288

144

FIGURE 3

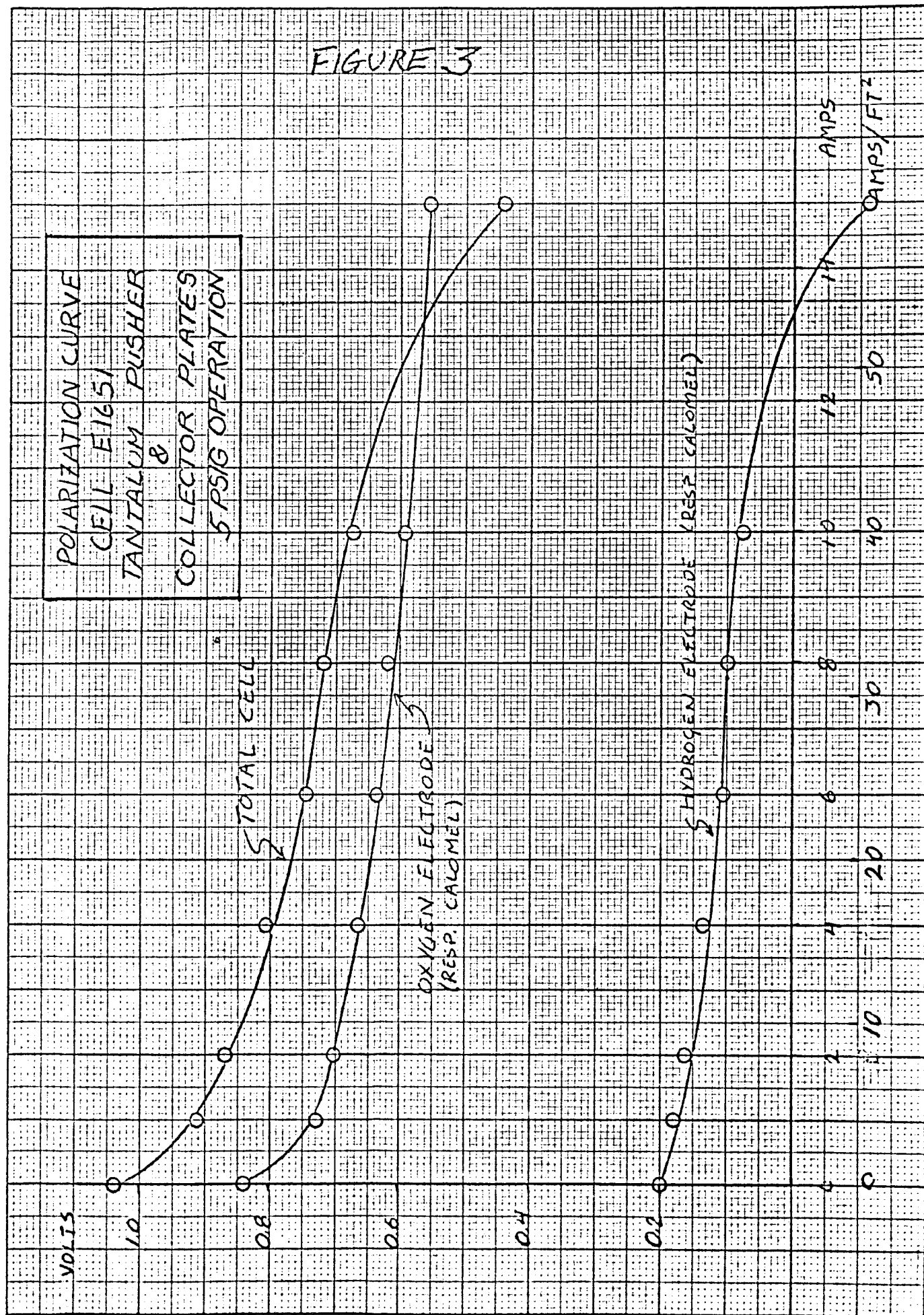


TABLE 2

Single 36 Sq. In. Cell Tests

Cell No.	Cell Components	Temp. °C.	Press. PSIG	Amps	Average Voltage	Time Hours	Spec. Cond. M /Ft. 2	REMARKS
E1279	Sintered Kel-F Electrode Std. Memb.	60	16	4.0	0.548 0.602 0.602 *0.712 **0.570	4 24 48 66 87	84	*Cell restarted after being shut down 140 hours due to malfunction in control system. **Recorded after cell had been off test 144 hours and restarted. Test discontinued due to poor performance after restarting.
E1282	Paste Electrode Std. Memb.	60	5	4.0	0.772 0.782 0.762 0.755 0.755 0.740 *0.780 0.780 0.758 0.744 0.728 0.748 0.700 -	5 24 46 72 96 120 123 144 216 240 264 288 312 384	145 123 109 109 79	*Recorded after cell had been shut off 72 hours and restarted. Cell test discontinued due to blockage of H ₂ outlet channel.
E1292	Sintered Kel-F Electrode Std. Memb.	30	16	4.0	0.762 0.780 0.702 0.598 0.638	4 24 48 72 144	121 125 65	Cell discontinued following 100 hours of operation. Except for accumulations of liquid in gas compartments, no changes were noted as a result of operation.

TABLE 2 (Cont'd)

Single 36 Sq. In. Cell Tests

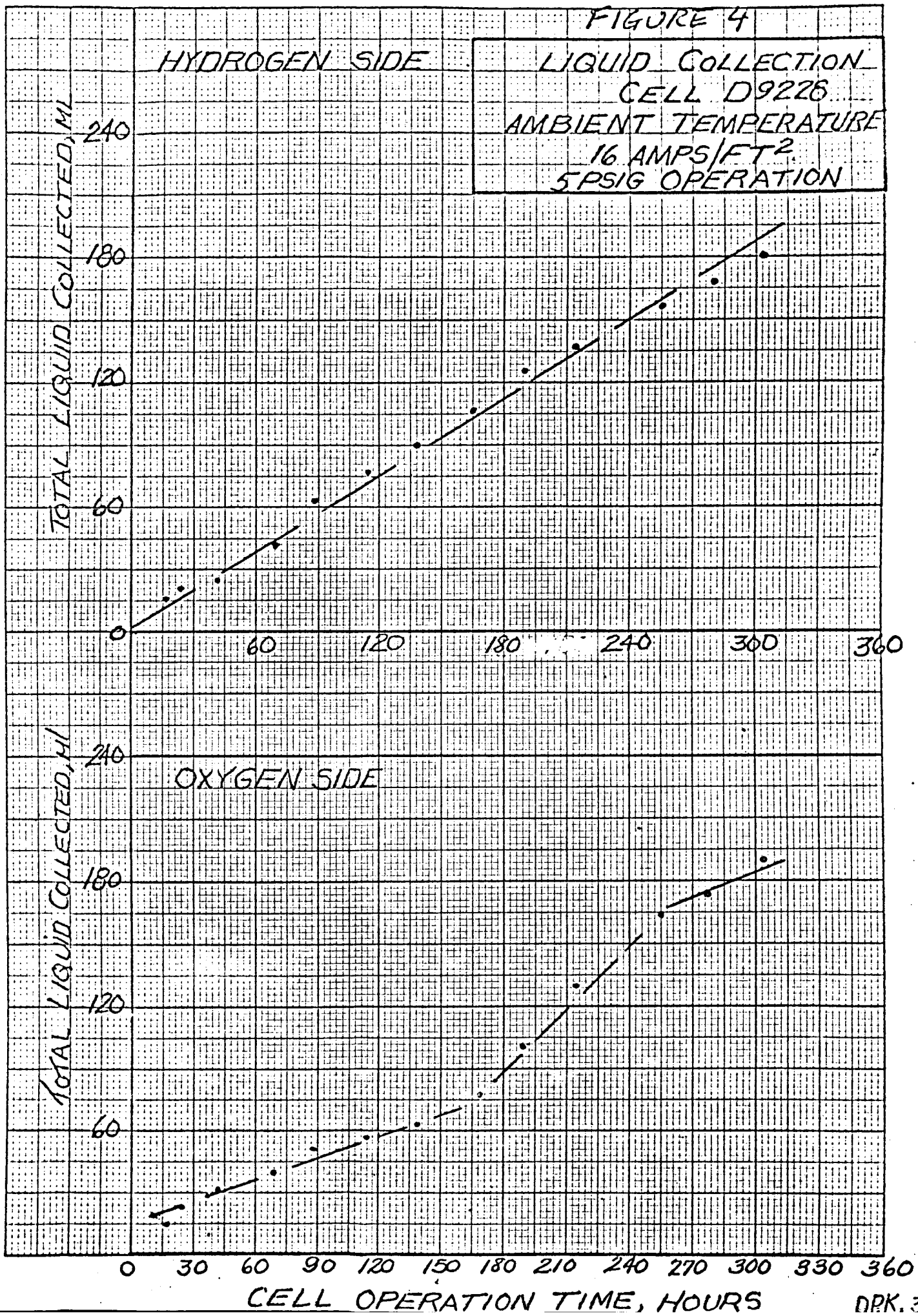
Cell No.	Cell Components	Temp. °C.	Press. PSIG	Amps	Average Voltage	Time Hours	Spec. Cond. Mhos/Ft. ²	REMARKS
E1651	Sintered (Teflon) Electrode Std. Memb. Tantalum Pusher of Collector Plates	60	5	4.0	0.812	4	266	Still Running
					0.802	24		
					0.848	48		
					0.847	72	178	
					0.826	96		
					0.808	168		
					0.808	192	182	
					0.782	240		
					0.768	288		
					0.813	336		
					0.791	360	132	
					0.785	384		
					0.812	408		
E1652	Sintered (Teflon) Electrode Std. Memb. Externally Fed PVC Electrolyte Compartment	60	1	4.0	0.648	8		*Cell is run only during day. Still running
					0.382	10		
					0.288	20		
					0.578	28		
					0.538	46		
					0.692	64		
					0.632	70		
					0.768	76		
					0.738	84		
					0.607	92		
					0.728	100		
					0.738	108		

TABLE 2 (CONT'D)

Single 36 Sq. In. Cell Tests

Cell No.	Cell Components	Temp. °C.	Press. PSIG	Amps	Average Voltage	Time Hours	Spec. Cond. Mhos/Ft. ²	REMARKS				
D9228	Sintered (Teflon) Electrode	Room Temp.	5	4.0	0.783	2	158	Still Running				
					0.716	48						
					0.742	72						
					0.772	96						
	Std. Memb.				0.746	120	129					
					0.738	144						
					0.756	168						
					0.728	192						
	Tantalum Pusher and Collector Plates				0.725	216	98					
					0.728	264			102			

FIGURE 4



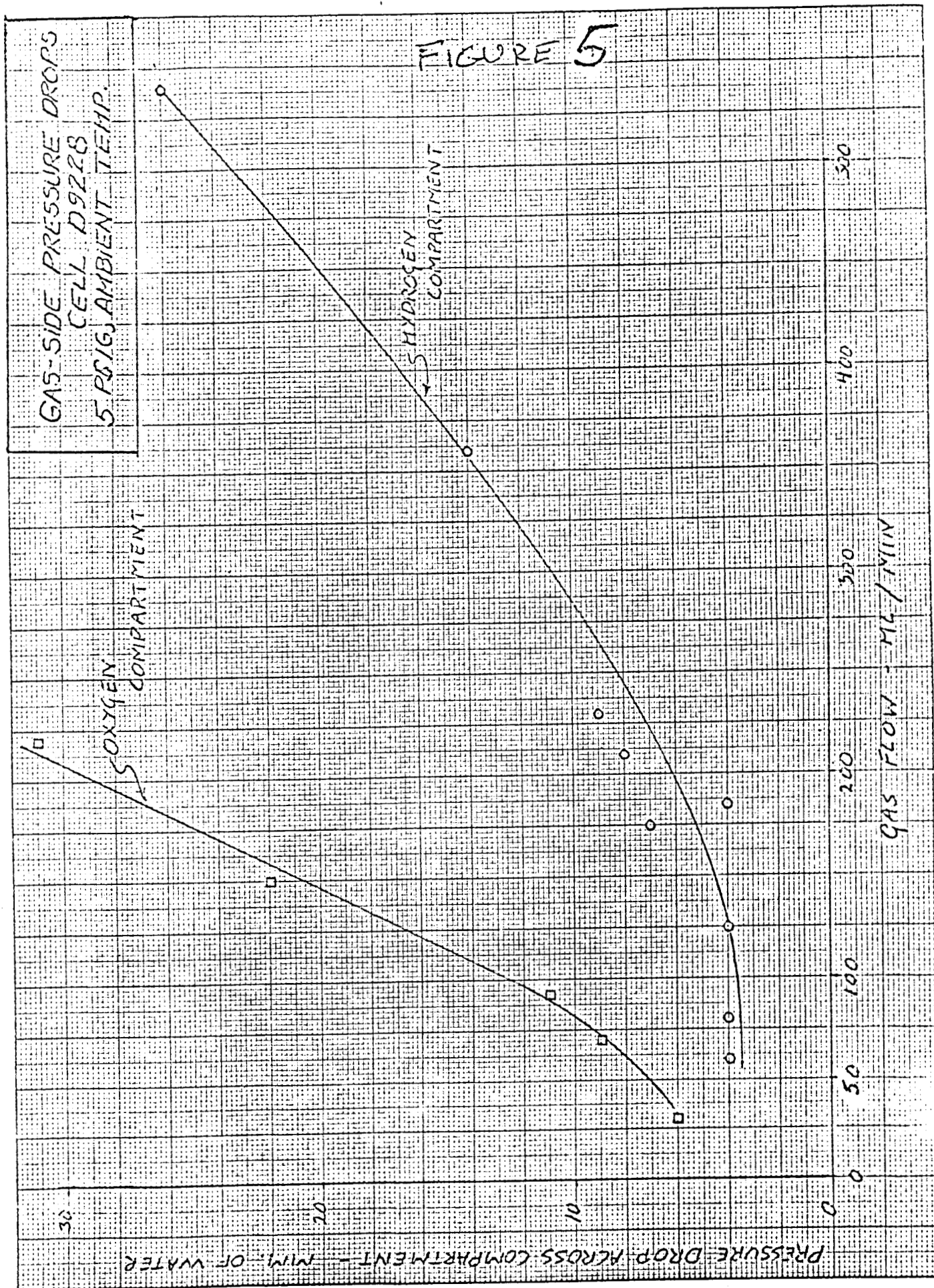


FIGURE 6

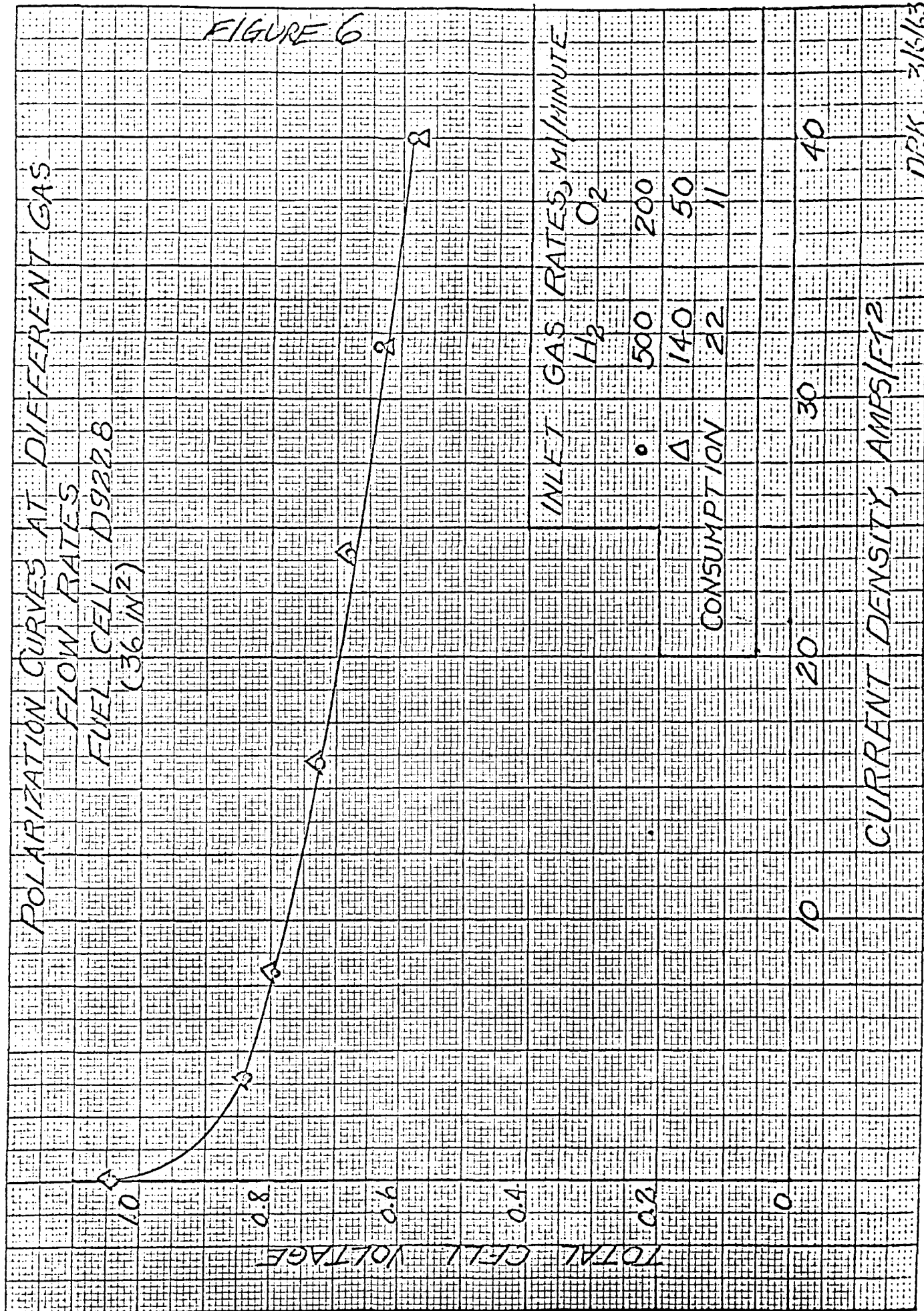


TABLE 3

Status of Components for 5-Cell Batteries

COMPONENT	QTY	MATERIAL	ORDERED	RECEIVED	DELIVERY DATE	FABRICATION SENT REC'D	OK FOR ASSEMBLY
End Plates	6	Stainless Steel	Yes	Yes		Yes	Yes
Tie Bolts	36	Stainless Steel	Yes	Yes		Yes	Yes
Nuts & Washers	72	Stainless Steel	Yes	Yes		Yes	Yes
Springs	36	Stainless Steel	Yes	Yes		Yes	Yes
Gas Compartments	20	Penton	Yes	No	15 March	No	No
	20	Halon	Yes	No	15 March	No	No
Electrolyte Compartments	10	Penton	Yes	No	15 March	No	No
	10	Halon	Yes	No	15 March	No	No
Gaskets	90	on-Dacron	Yes	Yes		Yes	Yes
	60	Buna N	Yes	Yes		No	No
Insulators	6	Butyl Rubber	Yes	Yes		Yes	Yes
Pusher Plates	20	0.010" Tantalum	Yes	No	11 March	No	No
	4	0.010" Niobium	Yes	Yes		4 March	No
	8	Zirconium	Yes	Yes		4 March	No
Separator Plates	20	Tantalum	Yes	No	11 March	No	No
	4	Niobium	Yes	Yes		4 March	No
	8	Zirconium	Yes	Yes		4 March	No
Electrodes	30	80 Mesh Platinum	Yes	Yes		No	No
Gauze	630	Platinum Black	Yes	Yes		No	No
Catalyst							
Membranes	20	61 AZG	Yes	No	14 March	No	No
	20	61 AZL	Yes	No	14 March	No	No

Thompson Ramo Wooldridge Inc.

	T1 H2SO4 IN °F	T2 H2SO4 OUT °F	VACUUM PRESS. IN HG	CIR H2O °F	VAC LINE VAC. °F	T3 OF °F	FRW	H2O CONDENSED CC	PH
1230	START	T2 SET ON FLOW							
1320	PURGE								
1342	PURGE FROM		30.0 TO	34.9	SLIGHT	WINT CONDENSATE ON CONDENSE			
1345	132.0	129.0	34.7	80.0	190/169	118/120	3.0	0	
1357	PURGE FROM		30.5 TO	34.0					
1400	127.5	126.0	34.0	80.0	190/170	118/120	3.0	.4	1
1412	PURGE FROM		30.7 TO	34.8					
1415	124.0	123.0	34.3	80.5	190/174	118/117	3.0	.3	1
1427	PURGE FROM		30.7 TO	34.6					
1442	PURGE FROM		31.0 TO	34.6					
1445	127.5	125.5	33.7	80.0	193/179	118/119	3.0	.5	1
1450	PURGE FROM		31.0 TO	34.6					
1500	PURGE FROM		31.5 TO	34.5					
1505	131.0	129.0	32.4	87.5	194/182	120/121	3.0		
1527	PURGE FROM		32.5 TO	33.5					
1530	141.5	139.5	33.0	98.5	193/188	128/127	3.0		
1542	PURGE FROM		33.5 TO	34.0					
1545	141.0	140.0	32.8	100.5	192/182	131/132	3.0	.5	1
1557	PURGE FROM		33.7 TO	34.5					
1600	139.5	137.5	32.0	100.5	192/182	130/131	3.0		
1612	PURGE FROM		34.1 TO	34.5					
1615	140.5	139.0	33.0	100.0	190/182	130/131	3.0		
1627	PURGE FROM		33.0 TO	34.5					
1630	142.0	140.5	32.8	100.0	192/181	132/130	3.0	.6	1
	STOP								
TITLE PERFORMANCE TEST #30								ENGR. TH	
BUBBLE FLOW READING 79.19 CM HG 374°F								OK	
MHI 3149 TONAR MEMBRANE #18								DATE 2-6-62	
								TEST NO. 03149-1-1	
								PROJECT 5-2-2-2-4	
FLUID H2SO4 20% 2-30									

Thompson Ramo Wooldridge Inc.

TIME	T1 14000 14000	T2 14000 14000	V1 14000 14000	V2 14000 14000	T3 14000 14000	FLOW 14000 14000	TEMP 14000 14000	
0730	152.0	146.0	32.5	77.0	190/142	127/120	3.0	.7 4
0747	152.0	146.0	32.5	77.0	190/142	127/120	3.0	.7 4
0750	152.0	146.0	32.5	77.0	190/142	127/120	3.0	.7 4
0827	152.0	146.0	32.5	77.0	190/142	127/120	3.0	.7 4
0840	174.0	166.0	32.7	82.0	190/152	146/150	3.0	10.7 5
0856	174.0	166.0	32.7	82.0	190/152	146/150	3.0	10.7 5
0905	174.0	163.5	32.5	81.0	190/152	146/150	3.0	10.7 5
1112	178.5	173.0	33.1	80.0	190/175	158/159	3.0	25.0 5
1127	178.5	173.0	33.1	80.0	190/175	158/159	3.0	25.0 5
1130	177.0	173.0	33.5	81.0	190/170	157/160	3.0	
1142	177.5	173.0	34.0	81.0	190/181	157/160	3.0	
1145	177.5	173.0	34.0	81.0	190/181	157/160	3.0	
1157	178.5	173.5	34.1	80.0	190/192	158/162	3.0	
1200	178.5	173.5	34.1	80.0	190/192	158/162	3.0	
1212	177.0	173.0	34.2	80.0	190/196	158/162	3.0	
1215	177.0	173.0	34.2	80.0	190/196	158/162	3.0	
1227	178.5	173.0	34.5	80.0	190/196	158/162	3.0	56.0 5
1230	178.5	173.0	34.5	80.0	190/196	158/162	3.0	56.0 5
1242	174.5	174.5	34.5	81.0	190/201	160/163	3.0	
1245	174.5	174.5	34.5	81.0	190/201	160/163	3.0	
1257	177.5	172.5	34.5	80.0	190/201	160/163	3.0	
1300	177.5	172.5	34.5	80.0	190/201	160/163	3.0	
1312	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1315	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1327	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1330	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1342	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1345	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1357	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1400	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1412	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1415	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1427	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1430	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1442	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1445	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1457	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1500	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1512	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1515	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1527	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1530	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1542	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1545	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1557	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1600	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1612	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1615	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1627	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1630	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1642	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1645	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1657	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1700	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1712	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1715	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1727	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1730	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1742	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1745	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1757	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1800	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1812	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1815	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1827	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1830	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1842	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1845	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1857	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1900	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1912	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1915	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1927	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1930	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1942	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1945	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
1957	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2000	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2012	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2015	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2027	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2030	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2042	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2045	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2057	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2100	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2112	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2115	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2127	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2130	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2142	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2145	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2157	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2200	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2212	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2215	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2227	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2230	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2242	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2245	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2257	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2300	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2312	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2315	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2327	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2330	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2342	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2345	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2357	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2400	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2412	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2415	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2427	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2430	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2442	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2445	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2457	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2500	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2512	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2515	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2527	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2530	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2542	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2545	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2557	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2600	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2612	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2615	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2627	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2630	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5
2642	177.5	173.5	34.5	80.0	190/201	160/163	3.0	56.0 5

TIME	IN °F	OUT °F	VACUUM PRESS	TEMP °F	VAC. LINE VAC. OF INCH	TEMP °F	FLOW	H ₂ O CONDENSED	PH
1215	SETTING CONDITIONS - 100% RH - 31								
	ADD 50 CC DIST H ₂ O TO H ₂ SO ₄								
1237	PURGE FROM	27.0	34.5						
	ADD 25 CC DIST H ₂ O TO H ₂ SO ₄								
1242	PURGE FROM	32.0	35.0						
1245	214.0	195.0	34.5	80.0	200/205	174/178	3.0	31.0	5
1257	PURGE FROM	29.0	35.0						
1400	205.0	198.5	34.5	80.0	204/212	180/184	3.0		
1412	PURGE FROM	29.0	35.2						
1415	201.5	195.5	34.5	80.0	205/213	178/182	3.0		
1427	PURGE FROM	30.0	35.2						
1430	202.0	195.0	34.5	80.0	205/214	178/182	3.0		
1442	PURGE FROM	20.5	35.2						
1405	203.5	197.5	34.7	80.0	200/216	177/182	3.0		
	CHANGE SAMPLE TO							69.5	5
	ADD 50 CC DIST H ₂ O TO H ₂ SO ₄								
1457	PURGE FROM	30.6	35.2						
1500	202.5	195.0	34.8	80.0	206/217	179/184	3.0		
1512	PURGE FROM	30.8	35.2						
1515	201.5	195.0	34.7	80.0	206/218	178/182	3.0		
1527	PURGE FROM	31.0	35.2						
1530	203.0	196.5	34.8	80.0	206/220	179/183	3.0		
1542	PURGE FROM	31.5	35.2						
1545	204.0	197.5	34.8	80.0	206/222	180/184	3.0		
	CONTINUE TO CONDITIONS FOR PER. TEST # 32							68.0	
	EXTRACTED 137.5 CC 4.0 PH-5								
	SLIDE COMPARATOR PH 4.5								
TITLE PERMANENCE TEST # 32								ENGR. TH	
STARTING READING 75.02 CM 15.21°F								JK	
2.60 INCH AMP 15.21°F								DATE 2-11-63	
ELEC TEMP 20°F								TEST NO. 2-11-63	
VAP PRESS 34.8 CM H ₂ O								PROJECT 52-02-224	
FLUID H ₂ O 10% SOLN									

Thompson Ramo Wooldridge Inc.

TIME	A. H ₂ O IN OF	T ₂ H ₂ O OUT OF	VACUUM PRESS CM HG	CIP 1/2 IN OF	VAC LINE OF	T ₂ OF	TH OF	FLOW	H ₂ O CONDENSED CC	PH
1545	SETTING CONTROLS - CONTINUOUS					FRIM	TEST #3			
	ADD 25 CC DIST H ₂ O TO H ₂ O									
1608	32.0	32.0	36.0							
1612	PURGE FROM 32.0 TO 36.5									
1615	204.0	198.0	36.0	40.0	205/220	181/185	3.0	33.0	5	
	ADD 25 CC DIST H ₂ O TO H ₂ O									
1627	PURGE FROM 32.0 TO 36.5									
1630	202.5	196.5	36.2	40.0	205/220	181/185	3.0			
1642	PURGE FROM 32.5 TO 36.5									
1645	202.5	197.0	36.2	40.0	206/222	181/185	3.0			
1657	PURGE FROM 32.5 TO 36.5									
1700	204.0	197.5	36.2	40.0	206/222	182/185	3.0			
	ADD 25 CC DIST H ₂ O TO H ₂ O									
1712	PURGE FROM 34.0 TO 36.5									
1715	203.0	197.0	36.2	40.0	206/224	181/185	3.0	66.0	5	
	CHANGE COLLECTOR									
1727	PURGE FROM 32.8 TO 36.5									
1730	203.0	197.0	36.2	40.0	206/224	181/185	3.0			
1742	PURGE FROM 33.2 TO 36.5									
1745	203.0	197.0	36.2	40.0	206/224	181/185	3.0			
	ADD 50 CC DIST H ₂ O TO H ₂ O									
1757	PURGE FROM 32.6 TO 36.5									
1800	202.0	196.0	36.2	40.0	206/224	180/185	3.0			
1812	PURGE FROM 32.6 TO 36.5									
1815	202.0	196.0	36.2	40.0	206/224	180/185	3.0	67.0		
	STOP									
	FILTERED 133.0									
	SCALE 250 MM HG									
TITLE PERFORMANCE TEST # 33									ENGR. TH	
BAROMETER CORRECTION 74.72 CM HG @ 71°F									OK	
C-60 CATION ANION MEMBRANE #10									DATE 2-11-68	
ELEC TEMP. 20.5°F									TEST NO. 000000	
FLUID H ₂ O									PROJECT 500-502028	

Thompson Ramo Wooldridge Inc.

TIME	T ₁ H ₂ O IN °F	T ₂ H ₂ O OUT °F	VAPOR PRESS PSIA	CIR. H ₂ O GPM	VAC. IN. IN. H ₂ O	T ₃ H ₂ O IN °F	FLOW GPM	H ₂ O EXTRACTED GPM	P.
0830	START	72.5	35.2	40.0					
0930	PURGE	FROM	32.0 TO	35.8					
0935	130.0	139.0	35.2	40.0	194/154	122/125	3.0	2.0	5
0942	PURGE	FROM	32.0 TO	36.0					
0945	154.0	147.0	35.3	38.0	192/162	124/127	3.0	9.0	5
* 0957	PURGE	FROM	32.5 TO	36.0					
1000	153.0	149.0	35.4	38.0	192/170	137/140	3.0	10.0	5
1012	PURGE	FROM	32.0 TO	36.2					
1015	151.0	147.5	35.5	38.0	191/178	137/140	3.0		
1027	PURGE	FROM	32.0 TO	36.0					
1036	151.5	143.0	35.5	38.0	191/184	137/139	3.0		
1042	PURGE	FROM	32.0 TO	36.1					
1045	152.0	148.5	35.5	38.0	191/190	137/140	3.0		
1057	PURGE	FROM	32.0 TO	36.1					
1100	150.5	144.0	35.5	38.0	191/193	138/141	3.0		
1112	PURGE	FROM	32.0 TO	36.0					
1115	153.0	150.0	35.4	38.0	191/196	139/142	3.0		
	H ₂ WENT UP 15CM THEN DOWN - ROCKED UP & DOWN								
	THEN SETTLED OUT - NO S. WENT								
1127	PURGE	FROM	32.1 TO	35.9					
1130	153.5	150.0	35.4	38.0	191/200	140/143	3.0		
	ADD TOSS OUT 1/20 TO H ₂ O								
1142	PURGE	FROM	32.5 TO	36.1					
1145	150.0	149.0	35.5	38.0	190/202	137/142	3.0		
1157	PURGE	FROM	32.9 TO	36.1					
1200	150.0	149.0	35.5	38.0	190/204	132/142	3.0		
	CONTINUE TO SET CONDITIONS FOR PT. 235								
	EXTRACTED 77.5 CC IN H ₂ O								
	SURE COMPRESSOR PT. 235								

TITLE PERFORMANCE TEST #34

EXTRACTOR READING 74.63 CM H₂O @ 71°F

MEMORANDUM

F.L.S. TEMP. 150°F

VAPOR PRESS. 35.5 CM H₂OFLUID H₂O OUT 80°F

ENGR. TH

K

DATE 5-1-57

TEST NO. 0510210 20

PROJECT 2-22-57

Thompson Ramo Wooldridge Inc.

[illegible]

TIME	T1 H2SO4 °F	T2 H2SO4 °F	140MM PRESS. CM H ₂ O	S.K. H ₂ O "	VAC LINE H ₂ O "	VAC POT H ₂ O "	FLOW	H ₂ O TANK LEVEL "	PH
930	START	TO SET	2400	24.0					
1002	PURGE	FROM	31.6 TO	32.1					
1045	152.0	137.0	33.0	78.0	190/210	113/126	2.6	2.0	5
1057	PURGE	FROM	29.0 TO	24.0					
1100	140.0	176.0	33.2	80.0	200/214	153/160	2.6	29.0	5
1112	PURGE	FROM	24.0 TO	34.2					
1115	143.0	182.0	33.5	80.0	205/215	161/167	2.8	26.0	5
1127	PURGE	FROM	29.0 TO	24.2					
	ADD	75.0 CC	WATER	160 TO H ₂ SO ₄					
1142	PURGE	FROM	30.0 TO	29.3					
1145	205	192.0	33.7	80.0	208/210	170/180	2.8	57.0	5
	ADD	30.0 CC	WATER	160 TO H ₂ SO ₄					
1157	PURGE	FROM	29.0 TO	34.2					
1200	200.0	190.0	33.5	80.0	208/220	167/177	2.8		
1212	PURGE	FROM	29.5 TO	34.2					
1215	201.0	192.0	33.6	80.0	208/221	172/178	2.8		
	CHANGE	COLLECTOR						64.5	5
	ADD	50.0 CC	WATER	160 TO H ₂ SO ₄					
1227	PURGE	FROM	29.3 TO	34.4					
1230	202.0	190.5	33.7	80.0	207/222	171/172	2.8		
	ADD	25.0 CC	WATER	160 TO H ₂ SO ₄					
1242	PURGE	FROM	21.6 TO	34.4					
1245	202.0	193.0	33.7	80.0	207/222	174/181	2.9		
	CHANGE	COLLECTOR						61.0	5
	ADD	25.0 CC	WATER	160 TO H ₂ SO ₄					
1257	PURGE	FROM	29.3 TO	34.4					
1300	206.0	196.0	33.8	80.0	207/222	175/182	2.8		
	ADD	25.0 CC	WATER	160 TO H ₂ SO ₄					
1312	PURGE	FROM	29.5 TO	34.3					
1315	204.5	190.0	33.7	80.0	207/222	175/183	2.8		
	CHANGE	COLLECTOR						62.5	5
TITLE: DETERMINATION OF TIT # 36								ENGR. TH	
EXPERIMENT: 74.02 CM H ₂ O @ 20°C								J.R.	
CUB. METER AMF MEMORANDUM #16								DATE 2-14-61	
FILE: 76105								TEST NO. 580005 ST	
FLUID: H ₂ SO ₄ CONC: 20%								PROJECT 52-1224	
								PAGE 1 OF 2	

Thompson Ramo Wooldridge Inc.

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[illegible]

Thompson Ramo Wooldridge Inc.

TIME	T ₁ H2O IN °F	T ₂ H2O OUT °F	VACUUM IN. HG	CIR. H2O IN	VACUUM IN. HG	T ₃ T ₄ °F	FLOW	H2O CONDENSED CC	PH
1125	SETTLED								
1227	PURGE	FROM	22.0	96.0					
1230	158.0	141.0	23.5	96.0	203/176	123/127	2.7	6.0	5
1242	PURGE	FROM	29.0	31.0					
1245	190.5	174.0	20.2	106.0	208/180	154/158	2.9	16.0	1
	ADD	25 CC	OUT	1.4	1.04				
1357	PURGE	FROM	24.5	25.5					
1300	205.0	193.0	24.8	120.0	208/182	167/176	2.8	30.0	2
1312	PURGE	FROM	24.5	26.0					
1315	191.0	182.0	26.3	121.0	208/190	140/150	2.8	39.0	5
1327	PURGE	FROM	25.6	28.5					
1330	199.5	197.0	27.8	118.0	208/192	167/172	2.8	22.0	5
	ADD	50.0 CC	OUT	1.4	1.04				
1342	PURGE	FROM	25.4	27.5					
1345	203.5	193.0	26.8	120.0	207/194	173/172	2.8		
	ADD	20.0 CC	OUT	1.4	1.04				
1357	PURGE	FROM	25.4	27.4					
1400	204.0	193.0	26.8	120.0	200/195	174/173	2.8		
	ADD	50.0 CC	OUT	1.4	1.04				
	CHANGE COLLECTOR							24.0	5
	ADD	75.0 CC	OUT	1.4	1.04				
1412	PURGE	FROM	25.5	27.4					
1415	203.5	192.5	26.8	120.0	200/200	174/174	2.8		
1427	PURGE	FROM	25.3	27.4					
1430	203.5	192.0	26.9	120.0	200/200	176/181	2.8		
	ADD	50.0 CC	OUT	1.4	1.04				
	CHANGE COLLECTOR							63.0	5
1442	PURGE	FROM	25.5	27.5					
1445	203.5	194.0	26.9	120.0	210/201	176/181	2.5		
	ADD	25.0 CC	OUT	1.4	1.04				
	SLIDE COMPARTMENT								PH 4.3
TITLE	C-60 343.00 H2O CONDENSATE #10							ENGR.	TJ
	FURNITURE 75.65 CM IN @ 72°F								JK
	C-60 343.00 H2O CONDENSATE #10							DATE	1-15-74
	FLEET TEMP 205°F							TEST NO.	0000000000
	FLUID H2O							PROJECT	512 000000
	VACUUM 26.9 CM HG								
	PAGE 1 OF 1								

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Thompson Ramo Wooldridge Inc.

TIME	T ₁ H ₂ O IN °F	T ₂ H ₂ O OUT °F	VACUUM PRESS. CM H ₂ O	CIR H ₂ O °F	VAC LINE "F VAC MAIN OF	T ₃ OF	T ₄ OF	FLOW	1/20 CONDENSED CC	P.V.
1520	SETTING 2042.2015 - CONTINUE FROM TEST #38									
	ADD 50.0 CC DIST. H ₂ O TO 1534									
1542	PURGE FROM	24.5	TO 24.5							
	ADD 50.0 CC DIST. H ₂ O TO 1554									
1557	PURGE FROM	24.0	TO 23.0							
1600	205.0	194.5	22.1	140.0	210/204	179/182	2.8	64.5	5	
	ADD 50.0 CC DIST. H ₂ O TO 1610									
1612	PURGE FROM	21.0	TO 22.4							
1615	204.0	195.0	21.2	140.0	211/207	179/182	2.8			
1617	PURGE FROM	21.0	TO 22.5							
1630	222.0	194.0	22.3	140.0	211/208	179/182	2.8			
	CHANGE COLLECTOR								74.5	5
1642	PURGE FROM	21.6	TO 23.0							
1645	202.0	193.5	22.6	140.0	211/208	178/181	2.8			
	ADD 50.0 CC DIST. H ₂ O TO 1654									
1657	PURGE FROM	21.5	TO 23.0							
1700	206.0	192.0	22.4	140.0	211/208	180/183	2.8			
	ADD 50.0 CC DIST. H ₂ O TO 1710									
1712	PURGE FROM	21.6	TO 23.0							
1715	201.0	193.5	22.5	140.0	211/209	179/182	2.8			
	CHANGE COLLECTOR								68.0	5
	ADD 25.0 CC DIST. H ₂ O TO 1724									
1727	PURGE FROM	21.3	TO 23.0							
1730	205.0	195.5	22.2	140.0	211/209	180/183	2.9			
1742	PURGE FROM	21.2	TO 23.0							
1745	205.0	196.0	22.3	140.0	211/210	181/183	2.8			
	ADD 50.0 CC DIST. H ₂ O TO 1754									
1757	PURGE FROM	21.2	TO 22.0							
1800	200	197.5	22.2	140.0	211/210	181/183	2.8	91.5		
	CONTINUE TO SET CONDITIONS FOR TEST #40									
	EXTRACTED 234.0 CC L.P. PHASE								COMPARISON 16.5	
TITLE PERFORMANCE TEST #39									ENGR. T.H.	
PARAMETER RESULTS 75.52 CM H ₂ O @ 23.5°F									J.R.	
C-60 CATION ANION MEMBRANE #12									DATE 2-15-61	
FLEC TEMP 200°F									TEST NO. 050000000	
FLUID H ₂ O @ CONC 20%									PROJECT 5-1-100	
VAC. PRESS 22.3 CM H ₂ O										

Thompson Rame Woolridge Inc.

TIME	IN °F	OUT °F	VACUM PRESS. CM Hg	CIR 1/2" OF	VAC. LINE 1/2" VAL. DIAM	T ₁ OF	T ₂ OF	FLOW	H ₂ O CONDENSED CC	PH
1800	SETTING CONDITIONS CONTINUING FROM TEST #39									
	ADD 50.0 CC DIST. H ₂ O TO H ₂ SO ₄									
1812	PURGE FROM	19.5	To	21.5						
1825	PURGE FROM	19.0	To	18.0						
1828	204.0	197.0	16.5	160.0	21' 210	183	184	2.8	44.5	5
	ADD 50.0 CC DIST. H ₂ O TO H ₂ SO ₄									
1840	PURGE FROM	15.5	To	17.0						
1843	205.0	197.0	16.4	160.0	21' 211	184	184	2.8		
1855	PURGE FROM	15.7	To	17.0						
1858	206.0	199.0	16.4	160.0	212 212	185	186	2.8		
	ADD 25.0 CC DIST. H ₂ O TO H ₂ SO ₄									
1910	PURGE FROM	15.9	To	17.0						
1913	206.0	199.0	16.7	160.0	212 212	185	186	2.8		
1925	PURGE FROM	16.2	To	17.2						
1928	206.0	198.5	16.8	160.0	212 212	184	186	2.8		
	CHANGE COLLECTOR									
	ADD 50.0 CC DIST. H ₂ O TO H ₂ SO ₄									
1940	PURGE FROM	16.5	To	17.5						
1943	203.5	197.0	17.2	160.0	212 212	182	184	2.8		
1955	PURGE FROM	16.4	To	17.5						
1958	204.5	197.5	17.1	160.0	212 212	183	184	2.8		
	ADD 25.0 CC DIST. H ₂ O TO H ₂ SO ₄									
2010	PURGE FROM	16.5	To	17.5						
2012	204.0	197.0	17.1	160.0	212 212	183	184	2.8		
2025	PURGE FROM	16.6	To	17.7						
2028	204.0	197.0	17.3	159.5	212 212	183	184	2.8		
	STOP									
	EXTENDED 159.5 CC									
	LO. PH									
	SLIDE COMPARTMENT PH 4.2									
TITLE PERFORMANCE TEST #40									ENGR. <i>WJ</i>	
EVALUATED CONDENSED 75.90 CC. 1/2" & 70°F									DATE 2-18-63	
C-60 CATIONIC DYE MECHANISM #10									TEST NO. 200000000	
FLEC TEMP -60°F									PROJECT 500 3-27-63	
FLUID H ₂ SO ₄ CONC 20% VAC. PRESS. 17.1 CM Hg										

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TIME	T ₁ H/204 OF	T ₂ H/504 OF	VACUUM PRESS CM H ₂ O	CIR. H ₂ O OF	VAC. LINE OF VAC. MAN.	T ₃ OF	T ₄ OF	FLOW	WATER CONSUMED	P.H.
0915	SETTING	204.0	32.0	76.0	194	148	150	3.0	0	
1027	PURGE	FROM	32.0	76.0	194	148	150	3.0	0	
1030		180.0	34.0	76.0	194	148	150	3.0	0	
1092	PURGE	FROM	32.0	76.0	194	148	150	3.0	0	
1095		204.0	34.8	79.0	194	170	162	3.0	7.0	5
1127	PURGE	FROM	32.0	76.0	194	170	162	3.0	7.0	5
1100		204.0	34.8	80.0	201	176	183	3.0	7.5	5
1122	PURGE	FROM	32.5	76.0	201	176	183	3.0	7.5	5
1115		199.0	35.0	80.0	202	180	178	3.0		
1127	PURGE	FROM	35.1	76.0	202	180	178	3.0		
1130		206.0	34.9	80.0	202	180	178	3.0		
1142	PURGE	FROM	35.1	76.0	202	180	178	3.0		
1145		202.5	35.0	80.0	202	180	178	3.0		
1157	PURGE	FROM	35.1	76.0	202	180	178	3.0		
1200		202.0	35.0	80.0	202	180	178	3.0		
1212	PURGE	FROM	35.1	76.0	202	180	178	3.0		
1215		203.5	35.1	80.0	202	180	178	3.0		
1227	PURGE	FROM	35.1	76.0	202	180	178	3.0		
1230		205.0	35.1	80.0	202	180	178	3.0		
1242	PURGE	FROM	35.5	76.0	202	180	178	3.0		
1245		206.5	35.2	80.0	202	180	178	3.0		
1257	PURGE	FROM	35.5	76.0	202	180	178	3.0		
1300		205.0	35.2	80.0	202	180	178	3.0		
	CONTINUE TO SET CONDITIONS FOR TEST # 44									
	EXTENDED 49.0 CC L.A. P.H. 5									
	SLIDE COMPRESSOR 4.0									
TITLE PERFORMANCE TEST # 43									ENGR. T. J.	
BAROMETRIC PRESSURE 73.79 IN. HG									DATE 2-20-66	
C-60 COTTON NITRE MEMBRANE #16									TEST NO. 100000	
ELEC. TEMP 20.0°F									PROJECT 100000	
VAC. PRESS. 35.1 CM H ₂ O										
FLUID H ₂ O										

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Thompson Ramo Wooldridge Inc.

TIME	T ₁ H ₂ O IN °F	T ₂ H ₂ O OUT °F	VACUUM PRESS IN Hg	T ₃ H ₂ O °F	VAC. LINE IN 1741 °F	T ₄ OF T ₂ °F	TEMP °F	WATER IN GAL	PH
0830	START	TO SET COND TANKS							
0902	PURGE	FROM	21.0	24.0					
0945	182.0	164.0	34.0	90.0	200/166	192/152	3.0	0	
0957	PURGE	FROM	24.6	23.2					
1000	204.0	193.5	32.0	109.0	202/172	168/176	3.0	7.5	5
1027	PURGE	FROM	22.0	26.5					
1032	206.0	201.0	26.4	140.0	205/180	182/186	3.0	7.0	5
1042	PURGE	FROM	24.6	26.9					
1045	206.0	201.0	26.8	140.0	202/184	182/186	3.0		
1057	PURGE	FROM	25.2	27.2					
1100	205.5	201.0	27.0	139.5	209/188	182/187	3.0		
1112	PURGE	FROM	25.5	27.3					
1115	205.0	201.0	27.1	139.5	210/190	184/188	3.0		
1127	PURGE	FROM	25.2	27.3					
1130	205.5	201.0	27.1	140.0	210/192	184/188	3.0		
1142	PURGE	FROM	26.3	27.2					
1145	205.0	201.0	27.1	140.0	210/192	184/188	3.0		
1157	PURGE	FROM	25.9	27.3					
1200	205.0	201.5	27.0	140.0	209/192	184/188	3.0		
1212	PURGE	FROM	26.1	27.5					
1215	204.5	200.0	27.4	132.5	209/190	184/188	3.0		
1227	PURGE	FROM	26.7	27.5					
1230	204.0	200.0	27.2	140.0	208/192	184/188	3.0		
	CONTINUE TO SET COND TANKS FOR TEST #16								
	EXTRACTED 90.5 GC 12-11-62								
	SLIDE CONDENSER PH 4.0								
TITLE: FERRIC CHLORIDE TEST #45								ENGR. TH	
EQUIPMENT: CONDENSER 75.00 IN Hg & 200°F								JK	
DATE: 3-21-62								TEST NO. 1000000000	
PROJECT: 200-1-1-1									
FLUID: 200-1-1-1									

TITLE	PERFORMANCE TEST # 47	ENGR.	J. H.
	BAROMETER READING 75.12 3/11 19 52.15	DATE	2-27-62
	COR. CHAIN FOR MEASUREMENT # 16	TEST NO.	300-100
	FLUID	PROJECT	200-100

Thompson Ramo Wooldridge Inc.

[illegible]



TAPCO a division of
Thompson Ramo Wooldridge Inc.

FINANCIAL REPORT
for
FEBRUARY - 1963
(Contract NAS 3-2551)

Submitted by

NEW PRODUCT RESEARCH of TAPCO
(Attachment to Monthly Progress Report No. 8)



FINANCIAL REPORT
for
Contract NAS 3-2551
for
Period Ending February 28, 1963

	<u>Current Month</u>	<u>Total To Date</u>
TRW Engineering Hours	286.5	1697.0
TRW Costs and Commitments	\$ 4,595	\$ 26,680
Subcontractor Costs and Commitments	<u>14,220</u>	<u>121,985</u>
TOTAL	\$ 18,815	\$ 148,665

TIME	T ₁ H ₂ O IN °F	T ₂ H ₂ O OUT °F	VACUUM PRESS CM H ₂ O	CIR. H ₂ O °F	VAC. LINE OF VAC IN °F	T ₃ °F	T ₄ °F	PAV °F	H ₂ O CONDENSED G	PH
1230	SLIGHTLY CONDENSED - CONTINUING FROM TEST #45									
	ADD 50.0 CC DIST 120 TO H ₂ O									
1237	PURGE	FROM	21.2	TO 22.5						
1300	202.0	199.5	22.0	160.0	210/192	184	184	3.0	5.5	5
1312	PURGE	FROM	20.8	TO 22.0						
1315	204.5	200.5	21.7	160.0	211/196	186	186	3.0		
1327	PURGE	FROM	20.5	TO 22.0						
1330	206.0	201.0	21.6	160.0	212/198	187	190	3.0		
	NO CONDENSATE APPEARING ON CONDENSER									
1330	CONDENSATE APPEARING VAPOR PRESSURE OCCURRING									
1345	PURGE	FROM	21.0	TO 22.0						
1348	204.0	202.0	22.0	160.0	212/198	187	191	3.0		
	VAPOR PRESSURE WITHIN VAC									
1400	PURGE	FROM	22.0	TO 22.5						
1403	205.0	202.0	21.6	160.0	212/198	188	191	3.0		
1415	PURGE	FROM	20.6	TO 22.5						
1418	204.5	201.5	21.9	160.0	210/198	187	191	3.0		
1430	PURGE	FROM	21.0	TO 22.5						
1432	204.5	201.5	21.9	160.0	210/198	187	190	3.0		
1445	PURGE	FROM	21.5	TO 22.5						
1450	204.0	202.5	22.0	160.0	210/198	188	189	3.0		
1500	PURGE	FROM	21.5	TO 22.5						
1502	203.5	200.0	22.2	160.0	210/198	184	187	3.0		
1515	PURGE	FROM	21.7	TO 22.5						
1518	203.0	200.0	22.2	160.0	210/198	185	187	3.0		
1530	PURGE	FROM	21.4	TO 22.5						
1533	203.0	200.2	21.8	160.0	210/198	185	187	3.0		
	STOP									
	EXTRACT 2 12.0 CC 1A PH. 5									
TITLE PERFORMED TEST # 46									ENGR. TH	
SUBJECT: PLE. BLOWING 74-95 200 1/2 5 1/2 °F									ST	
C-60 CATH. RPT. MEMORANDUM #16									DATE 2-2-62	
TEST TEMP 200°F VAC PRESS. 2-0 CM H ₂ O									TEST NO. 2-222-2	
FLUID H ₂ O									PROJECT 2-222-2	